

# Comparative Analysis of FOC Based Three Level DCMLI Driven PMSM Drive

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**Abstract—** This paper deals with an comparative analysis of field-oriented control (FOC) based three level diode clamped multilevel inverter (DCMLI) driven Permanent Magnet Synchronous motor (PMSM) drive. The FOC of PMSM is widely used methods for the speed and torque control. The FOC PMSM drive system is designed simulated and implemented using various modulation techniques to calculate the desired torque, speed and stator current. The main disadvantage of Pulse Width Modulation (PWM) & Space Vector Modulation (SVM) are the problem of higher total harmonic distortion (THD) and lower effective DC utilization. In CBSVM, The main advantages of SVM is fast and efficient implementation, without sector determination & work on the effective time relocation algorithm. The Simulation analysis of the novel scheme is carried out by using MATLAB software. The simulation results show that the proposed novel control scheme has a good dynamic response in terms of speed and torque response. It can also reduce the torque ripple and THD of voltage and current gives better motor performance.

**Keywords—** Carrier Based Space Vector Modulation (CBSVM), Diode Clamped Multilevel Inverter (DCMLI), Field Oriented Control (FOC) Permanent Magnet Synchronous Motor (PMSM), Pulse Width Modulation (PWM), Space Vector Modulation (SVM), Total Harmonic Distortion (THD).

## I. INTRODUCTION

The main advantages of PMSM drives are reduced losses, motor size and use of reluctance torque hence overall efficiency improved over the induction motor. Recently for PMSM drive control, the different schemes are used having the good torque response and the FOC has been considered as best solution for torque control.[1]Multilevel inverter technology has played very important role in the area of high-power medium voltage energy control. For reducing THD as compared to conventional inverter, a new family of DCMLI has optimum solution to increase the voltage levels and lower harmonic distortion [2-3]. In three level DCMLI, clamping diodes can produce additional voltage level for reduces the harmonic distortion. A various modulation techniques have been discussed to control the inverter [4]. The main characteristics of CBSVM technique is used control variable directly for improving DC link voltage utilization, reducing THD and losses. The main objective of the FOC is achieved by using a direct and quadrature axis d-q reference frame and also the torque equation [5]. In DCMLI

inverter because of better gate pulses not only it gives better sinusoidal voltage or current also gives better speed control of machines [6].

In this paper, we presented a simple algorithm to perform the CBSVM for three level DCMLI. In CBSVM, it is run on concept of effective time to allow fast and efficient implementation of SVM without sector determination. So that the inverter output voltage is directly calculated in the effective times. It can be converted in a simple by effective time relocation method and based on the duty ratio profiles. In CBSVM, the common mode voltage injection method is used to generate [9-11].

## II. MATHEMATICAL MODEL OF PMSM

The PMSM model equations are:

$$V_d = RI_d + L_d(dI_d / dt) - P\omega L_q I_q \quad (1)$$

$$V_q = RI_q + L_q(dI_q / dt) + P\omega L_d I_d + P\omega\lambda_f \quad (2)$$

$$T_e = T_L + B\omega + J_m(d\omega / dt) \quad (3)$$

$$T_e = K_t I_q + (3/2)P(L_d - L_q)I_d I_q \quad (4)$$

In Surface mounted permanent magnet motor,  $L_d = L_q$

$$\text{So, } T_e = K_t I_q \quad (5)$$

$$K_t = (3/2)P\lambda_f \quad (6)$$

In equation (5) the torque producing current is along the q-axis current.

The d, q variables are converted in to a, b, c variables through the Park's transformation

$$\begin{bmatrix} V_q \\ V_d \\ V_0 \end{bmatrix} = \frac{2}{3} \begin{bmatrix} \cos\theta & \cos(\theta - 2\pi/3) & \cos(\theta + 2\pi/3) \\ \cos\theta & \cos(\theta - 2\pi/3) & \cos(\theta + 2\pi/3) \\ 1/2 & 1/2 & 1/2 \end{bmatrix} \begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix} \quad (7)$$

The inverse Parks transformation is defined below:

$$\begin{bmatrix} V_a \\ V_b \\ V_c \end{bmatrix} = \frac{2}{3} \begin{bmatrix} \cos \theta & \sin \theta & 1 \\ \cos(\theta - 2\pi/3) & \sin(\theta - 2\pi/3) & 1 \\ \cos(\theta + 2\pi/3) & \sin(\theta + 2\pi/3) & 1 \end{bmatrix} \begin{bmatrix} V_q \\ V_d \\ V_0 \end{bmatrix} \quad (8)$$

For a balanced system the power equation is:

$$V_a I_a + V_b I_b + V_c I_c = (3/2)(V_d I_d + V_q I_q) \quad (9)$$

### III. CONTROL TOPOLOGY

#### A. Field Oriented Control

In Block diagram of FOC- CBSVM based three level DCMLI PMSM drive, the measured voltages and currents into  $a-\beta$  reference frame are transform into  $d-q$  frame using Park transformation. The error is given to the PI controller after comparing the reference speed with the motor speed. The output of the PI controller is taken as  $q$ - axis current goes to current controller with reference  $i_d = 0$ . The reference waves and triangular waves compared and pulses are given three level DCMLI.

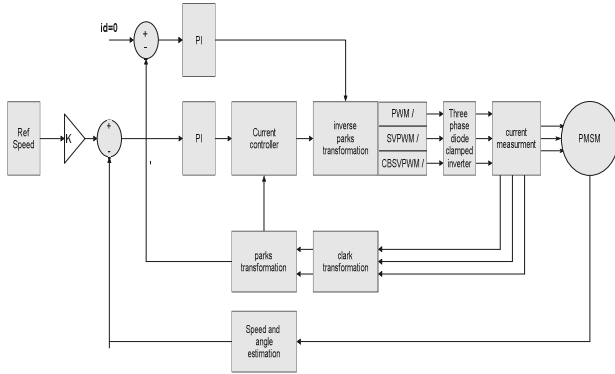


Fig. 1. Block diagram of FOC based three level DCMLI

#### B.

#### C. Multilevel Inverter Topology

The DCMLI comprises of two series-connected capacitors, C1 and C2, the DC-link capacitors which divide the DC bus voltage into three levels;  $+V_{dc}/2, 0$  &  $-V_{dc}/2$ . 'n' is the neutral point between two capacitors C1 and C2. (Sa1, Sa3) and (Sa2, Sa4) are two complementary switch pairs and (D1, D10) are the two clamping diodes per phase. Figure 2 shows the three-level DCMLI driven to PMSM drive. The switching sequence for the three level diode clamped inverter are shown in table-I

If Sa1 and Sa2 is ON, so  $V_{an} = +V_{dc}/2$ .

If Sa2 and Sa3 is ON, so  $V_{an} = 0$ .

If Sa3 and Sa4 is ON, so  $V_{an} = -V_{dc}/2$

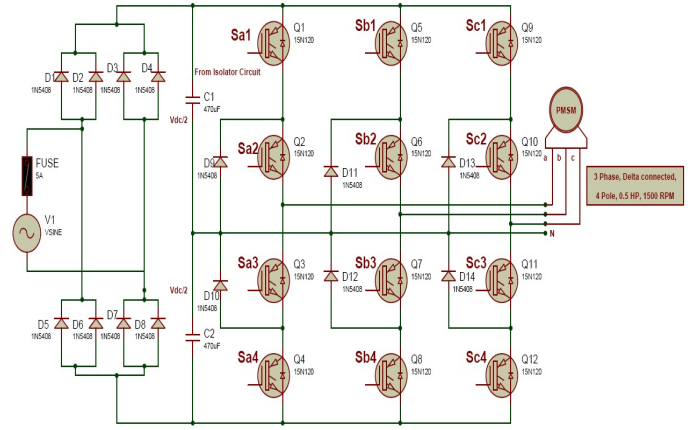


Fig. 2. Power circuit of three-level DCMLI driven PMSM

#### D. CBSVM Algorithm

In CBSVM there are four switches per phase of the three level inverter and two triangular carriers are required to be turned-on and -off complementarily. A universal representation of modulation signals are represented by

$$u_i(t) = u_i^*(t) + e_i(t) \quad (10)$$

$$u_i^*(t) = m \sin \omega t$$

$$u_b^*(t) = m \sin(\omega t + 2\pi/3)$$

$$u_c^*(t) = m \sin(\omega t + 4\pi/3) \quad (11)$$

Where  $m$  is the modulation index, and

$$u_a^*(t) + u_b^*(t) + u_c^*(t) = 0$$

$$U_a N(t) = [E/2][m \sin \omega t + e_i(t)]$$

$$U_b N(t) = [E/2][m \sin(\omega t + 2\pi/3) + e_i(t)]$$

$$U_c N(t) = [E/2][m \sin(\omega t + 2\pi/3) + e_i(t)] \quad (12)$$

$$U_{ab}(t) = U_a N(t) - U_b N(t) = [E/2][\sqrt{3}m \sin(\omega t + \pi/6)]$$

$$U_{bc}(t) = [E/2][\sqrt{3}m \sin(\omega t + 5\pi/6)]$$

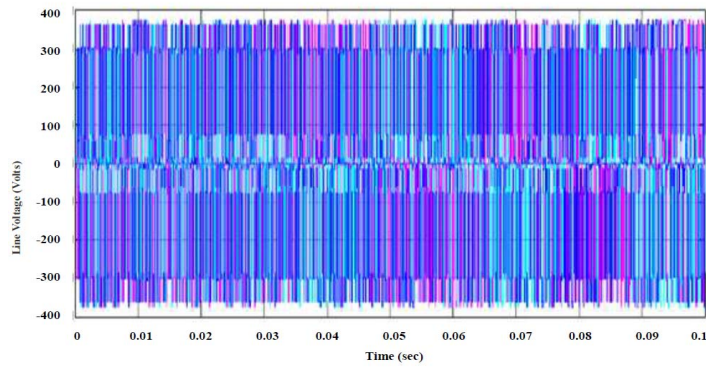
$$U_{ca}(t) = [E/2][\sqrt{3}m \sin(\omega t + 3\pi/6)] \quad (13)$$

It is clear that the injected harmonics do not appear in the line to line voltages.

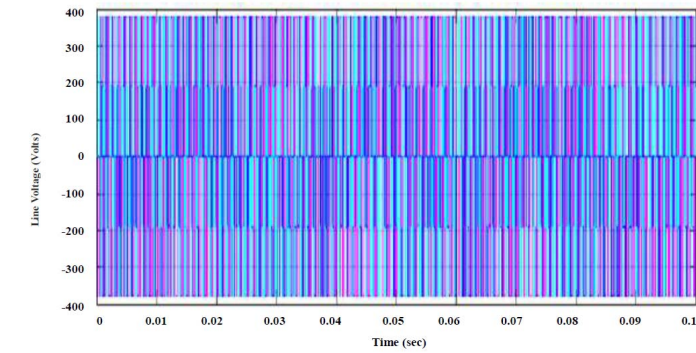
### IV. RESULTS ANALYSIS

The result analysis of FOC based three level DCMLI using CBSVM driven PMSM drive is find for the steady and transient condition. The outputs of CBSVM are shown from fig.5 to fig.8. Fig.9 to fig.10 Show the THD analysis of line voltage and phase current. Table I shows that torque ripple analysis of PMSM drive Table II show that the lower THD of three level DCMLI using CBSVM technique.

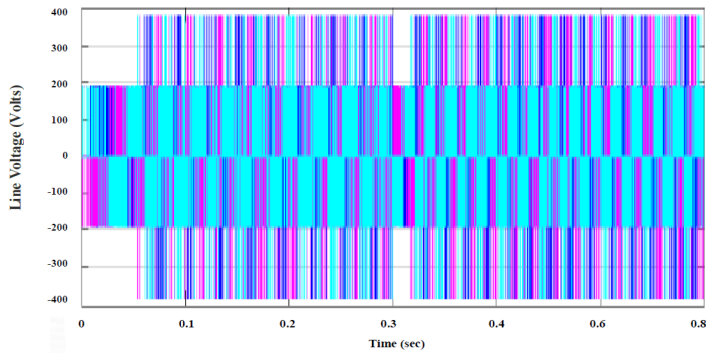
$L_d=0.006365H$ ;  $L_q=0.006365H$ ;  $R=1.6\Omega$ ;  
 $PM\_flux=0.1852Wb$ ;  $P=2$ ;  $F=0.00005396\text{ Nm-s}$ ;  
 $J=0.0001854\text{ Kgm}^2$



(a)

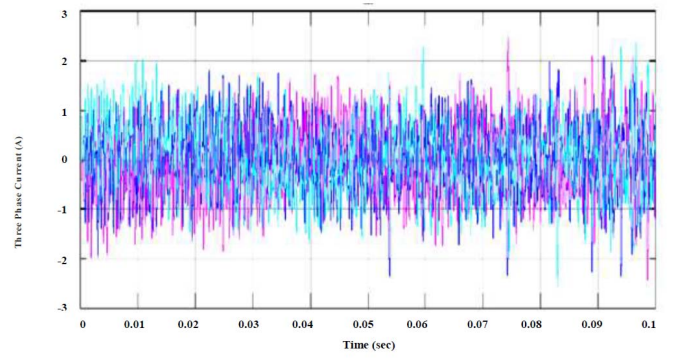


(b)

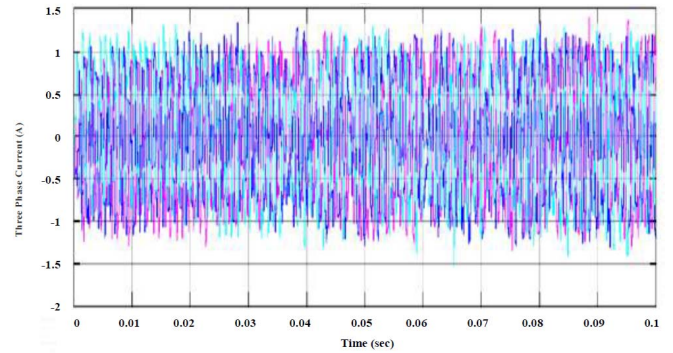


(c)

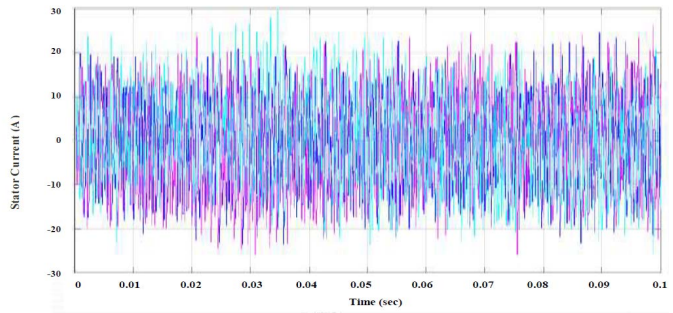
Fig. 3. Inverter voltage using (a) PWM (b) SVM (c) CBSVM



(a)

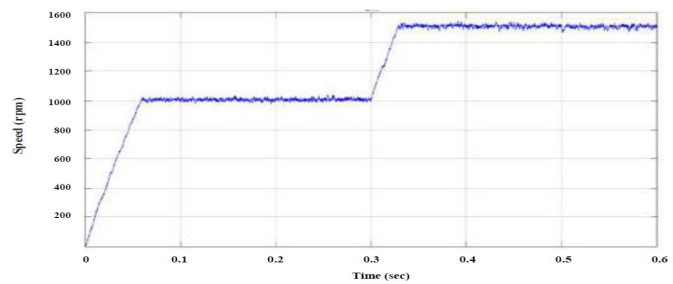


(b)

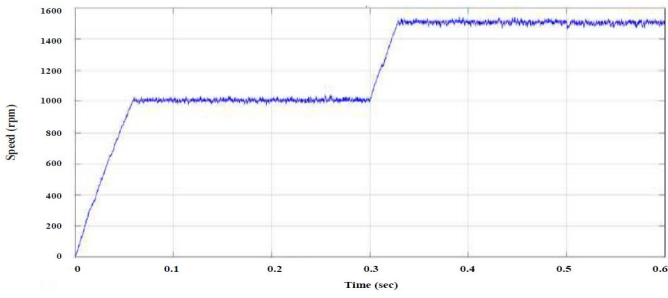


(c)

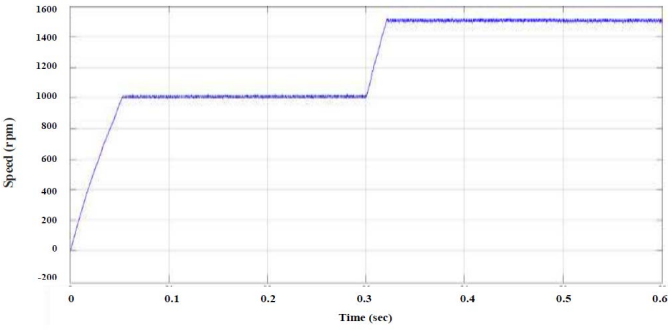
Fig. 4. Inverter current using (a) PWM (b) SVM (c) CBSVM



(a)

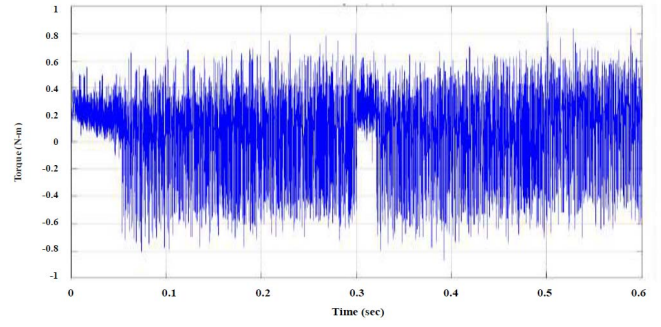


(b)



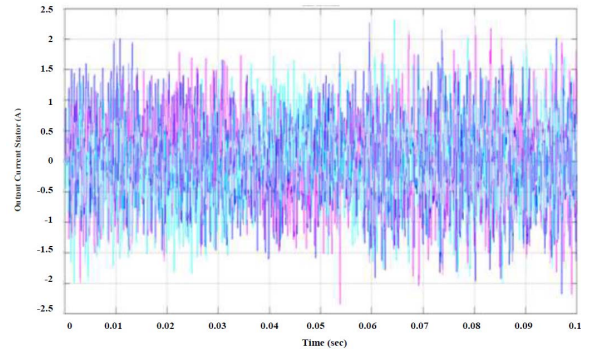
(c)

Fig. 5. Speed response using (a) PWM (b) SVM (C) CBSVM

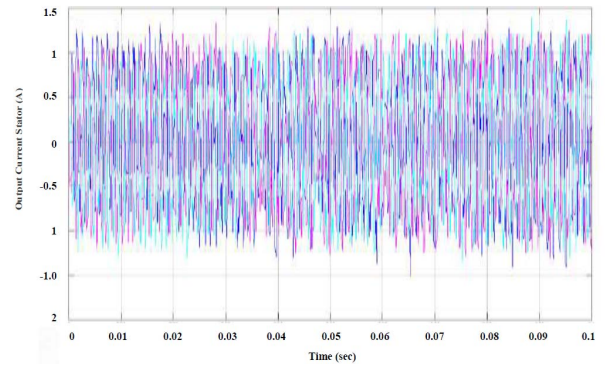


(c)

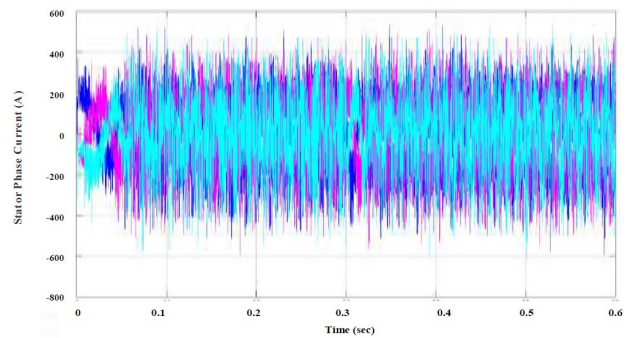
Fig. 6. Torque response using (a) PWM (b) SVM (C) CBSVM



(a)

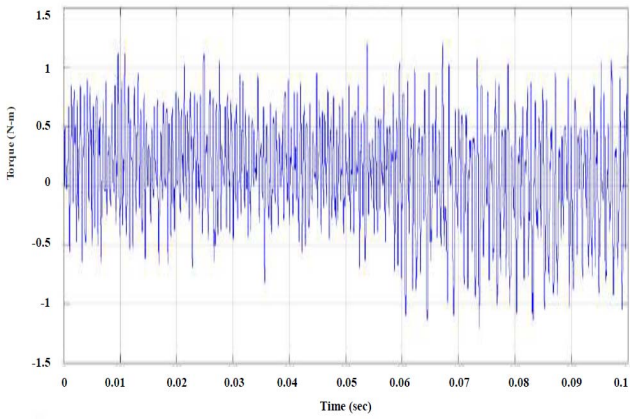


(b)

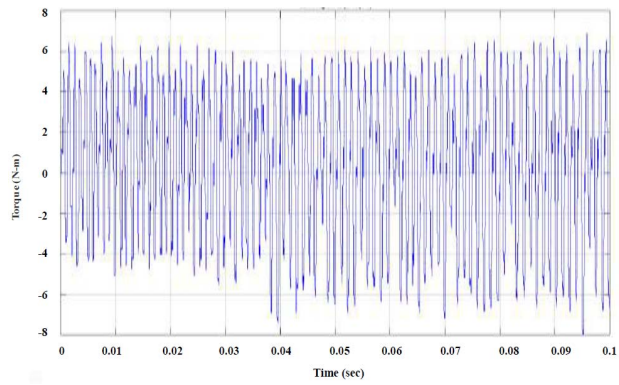


(c)

Fig. 7. Motor current using (a) PWM (b) SVM (C) CBSVM



(a)



(b)

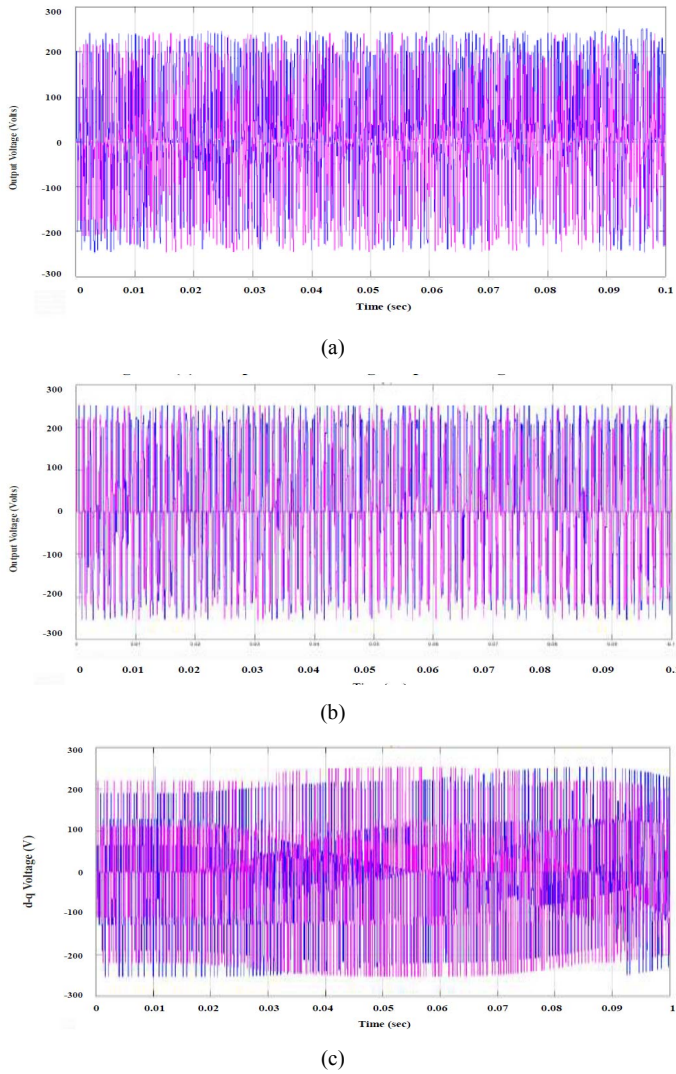
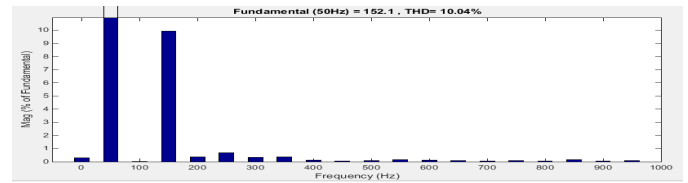
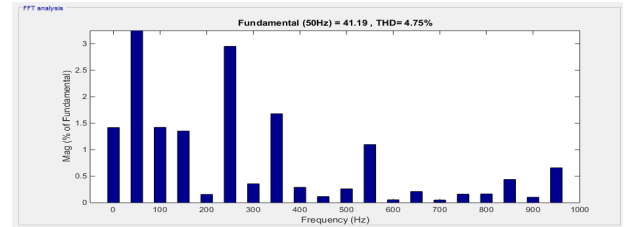


Fig. 8. D-Q voltage outputs using (a) PWM (b) SVM (C) CBSVM

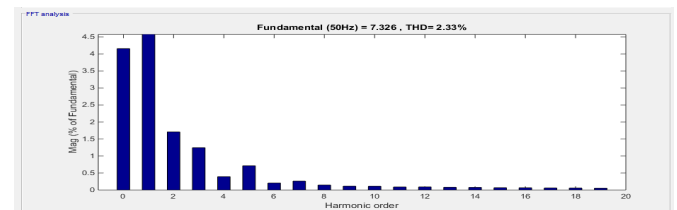


(c)

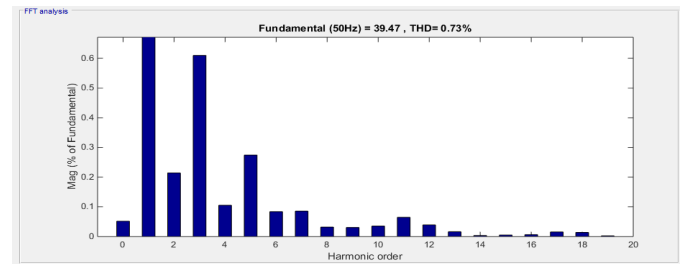
Fig.9. THD of line voltage using (a) PWM (b) SVM (C) CBSVM



(a)



(b)



(c)

Fig. 10. THD of Current using (a) PWM (b) SVM (C) CBSVM

Torque ripple can be calculated  

$$\% \text{Torque ripple} = (T_{max} - T_{min}) / T_{avg} * 100$$

TABLE I. TORQUE RIPPLE ANALYSIS

% Torque Ripples	Torque Analysis		
	PWM	SVM	CBSVM
20%		18%	15.38%

TABLE II. THD ANALYSIS

THD	THD Analysis		
	PWM	SVM	CBSVM
Line Voltage	89.74%	10.89%	10.04%
Line Current	4.75%	2.33%	0.73%

## V. CONCLUSION

The simulation analysis of FOC-CBSVM based three-level DCMLI driven PMSM drive has been studied in this paper. The comparative analysis of inverter voltage, current, speed, torque and the three-phase motor currents of the PMSM for PWM, SVM and CBSVM have plotted. It conclude that the FOC based three-level DCMLI driven PMSM using CBSVM gives better speed-torque characteristics compared to PWM and SVM techniques with less transients and good steady state response. The % torque ripple of FOC based three level DCMLI driven PMSM drive using novel CB-SVM technique is less as compare to PWM and SVM techniques' which in shown in table I.

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